

RHIC AC Dipole Preliminary Study

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Requirements:

- (1) Integrated dipole field = 100 G-m @ 39 kHz;
(sometimes @ 60kHz)

Aperture -- limited by ceramic vacuum pipe 4" (ID)
with 0.25" thickness wall \longrightarrow 4.5" (OD) = 11.43 cm
 \longrightarrow Clear bore: $R = 6.0$ cm (coils)

- (2) Field quality – low E-3 field errors within $R < 3$ cm

Goals: dipole $b_1 \sim 100$ Gauss ($L_m = 1$ m)
sextupole ratio $b_3/b_1 \sim 1.5E-3$ @ $R=2$ cm
 $3.4E-3$ @ $R=3$ cm
obey scaling $\sim (R/R_o)^{**2}$

(All cases in this study are achieved such quality)

Existing AC Dipole – Large current sheet type

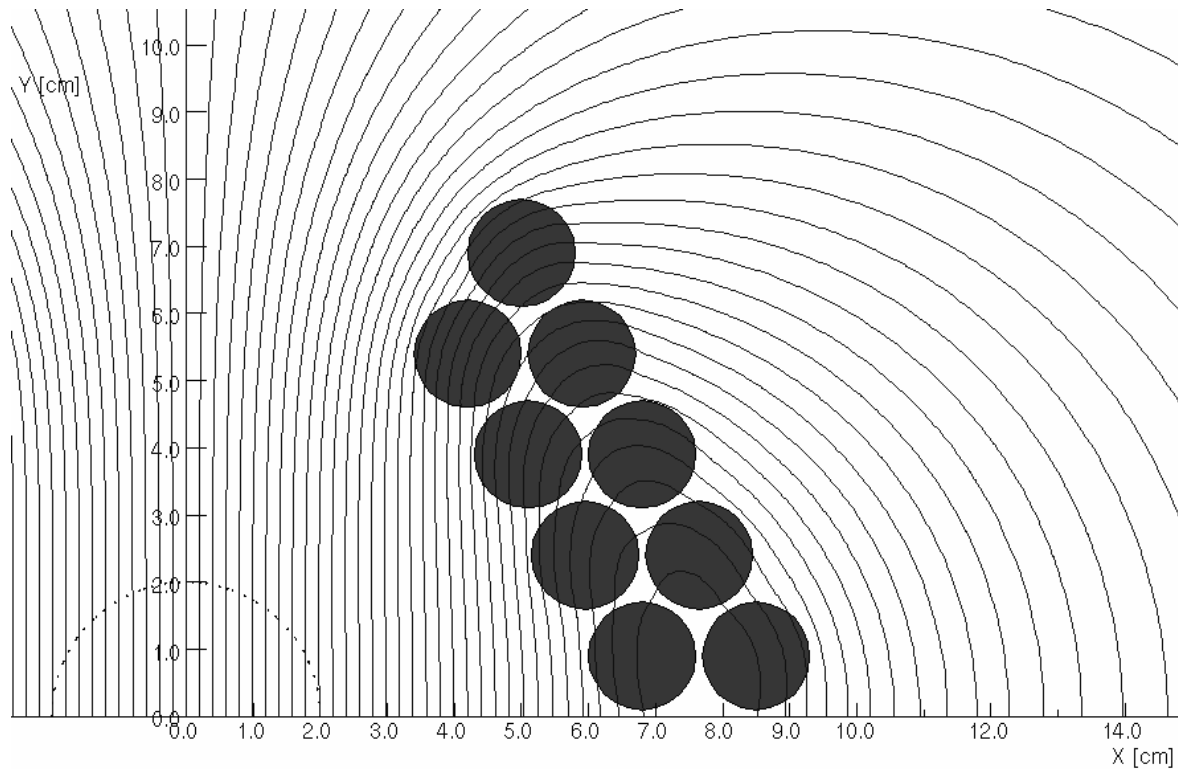
small aperture $\sim R=1.5$ cm; $I_0 = 79$ A

Good field quality (in 2d), but high inductance ~ 104 μ H

Scaled from Existing One –

If we use similar conductor, more turns ($N=8$, or 9) are needed to build up enough height to achieve field quality.

Scaled from existing one – Air-coil



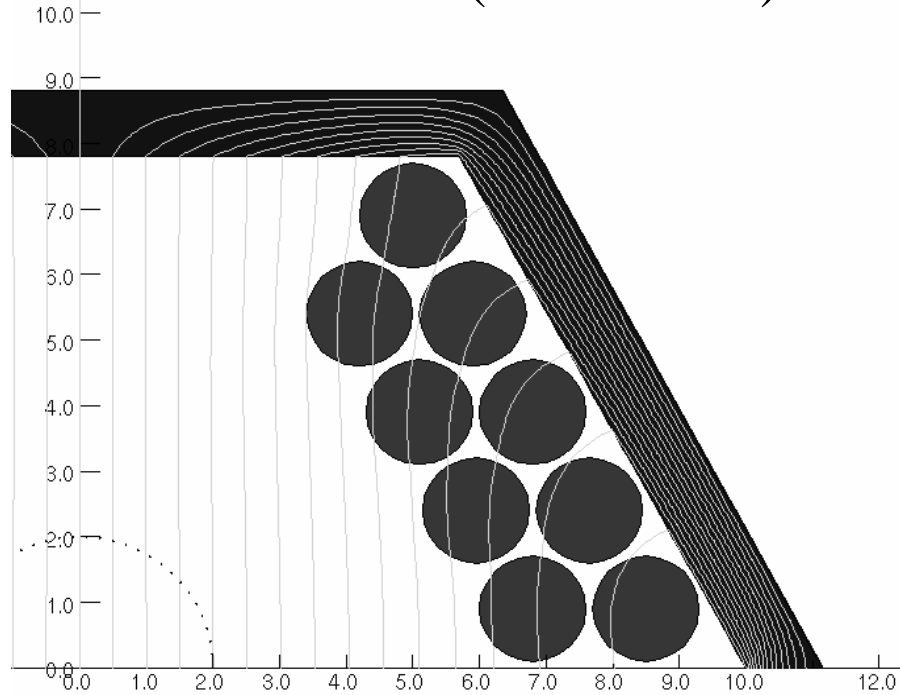
$$N = 9 \text{ (x2)}$$

$$I_0 = 127.15 \text{ A}$$

$$L = 153.7 \text{ } \mu\text{H}$$

(per magnet with $L_m = 100 \text{ cm}$)

Scaled with Ferrite (CMD5005)



$$N = 9 \text{ (x2)}$$

$$I_o = 69.7 \text{ A}$$

$$L = 296.4 \text{ } \mu\text{H}$$

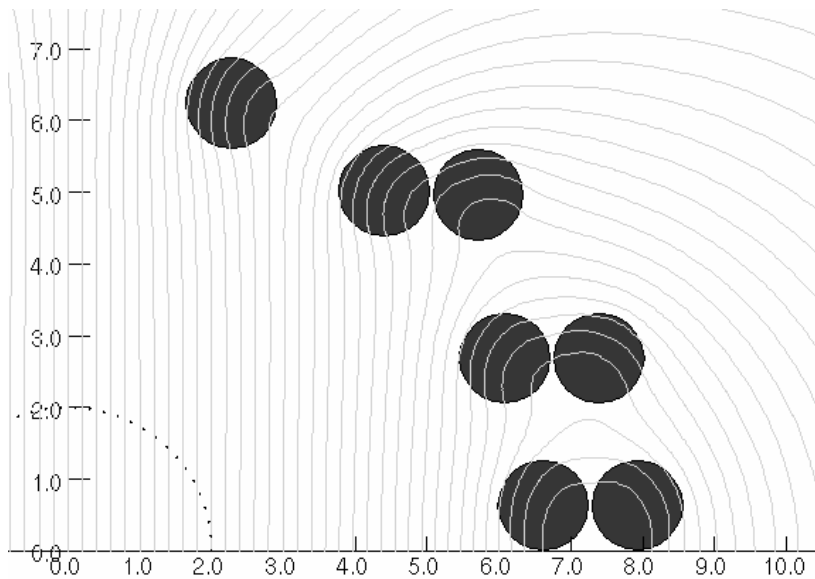
How to improve ?

Inductance can be reduced by reducing the number of turns

- (I) Cosine theta type (with/without ferrite shell);
- (II) Window-frame ferrite yoke, with thin Cu conductor;
(Cu skin depth: $d = 0.33 \text{ mm @ } 39 \text{ kHz}$)

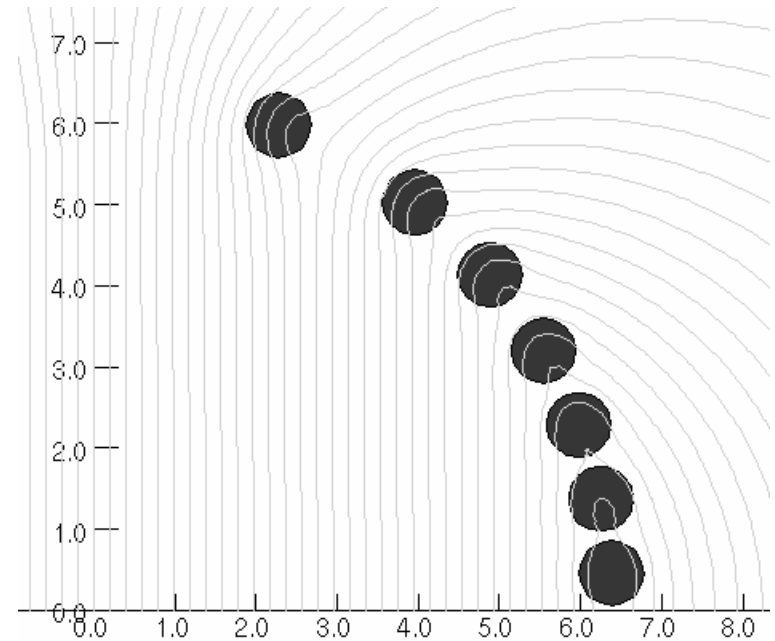
(I) Cosine Theta Type -- $N = 7$ (x2) Air-coil

Two-layer



$$I_0 = 162.7 \text{ A}$$
$$L = 90.7 \text{ } \mu\text{H}$$

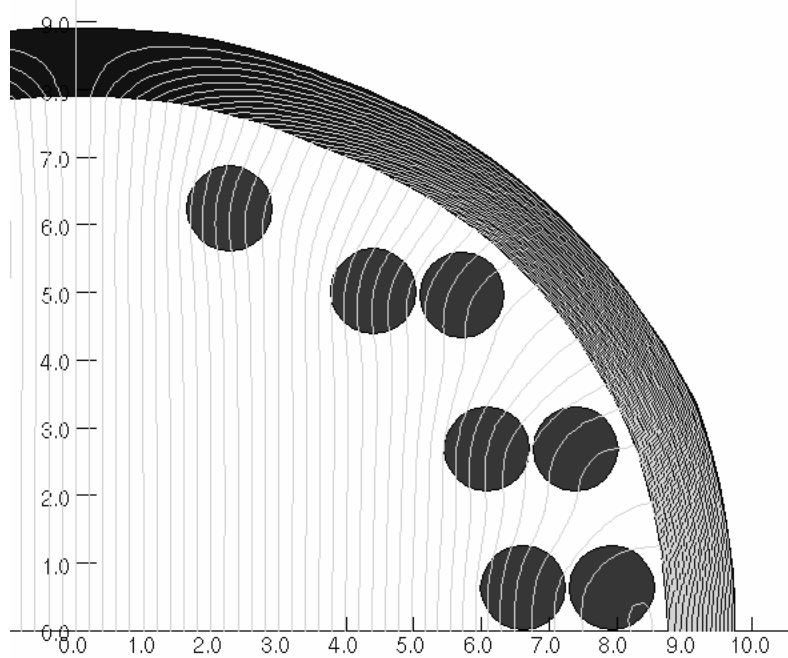
One-layer (small conductor)



$$I_0 = 149.7 \text{ A}$$
$$L = 93.3 \text{ } \mu\text{H}$$

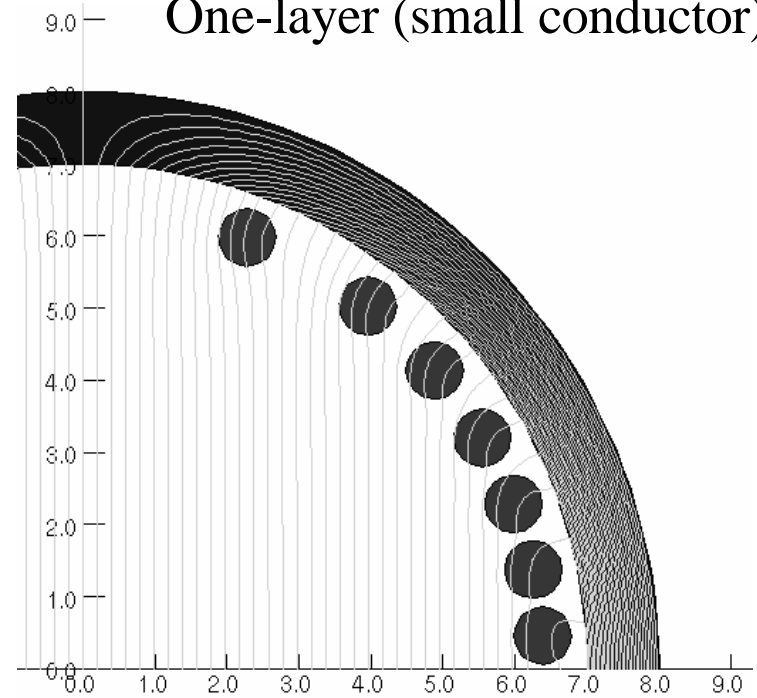
Cosine Theta Type -- $N = 7$ (x2) with Ferrite

Two-layer



$$I_0 = 89.8 \text{ A}$$
$$L = 171.1 \text{ } \mu\text{H}$$

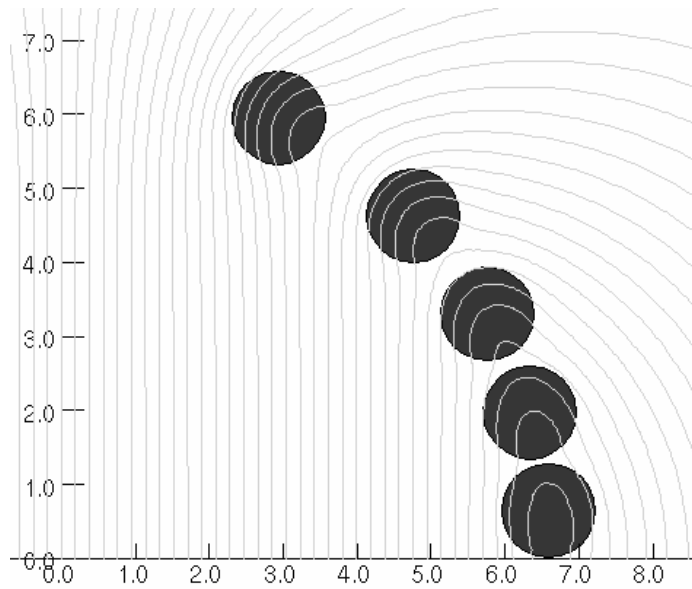
One-layer (small conductor)



$$I_0 = 79.9 \text{ A}$$
$$L = 175.8 \text{ } \mu\text{H}$$

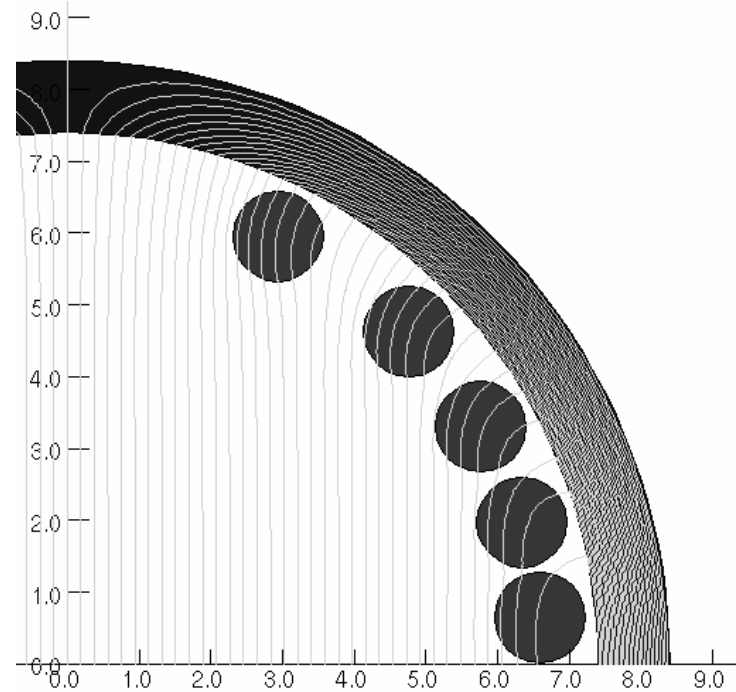
Cosine Theta Type – N=5 (x2)

Air-coil



$$I_0 = 223.0 \text{ A}$$
$$L = 47.53 \text{ } \mu\text{H}$$

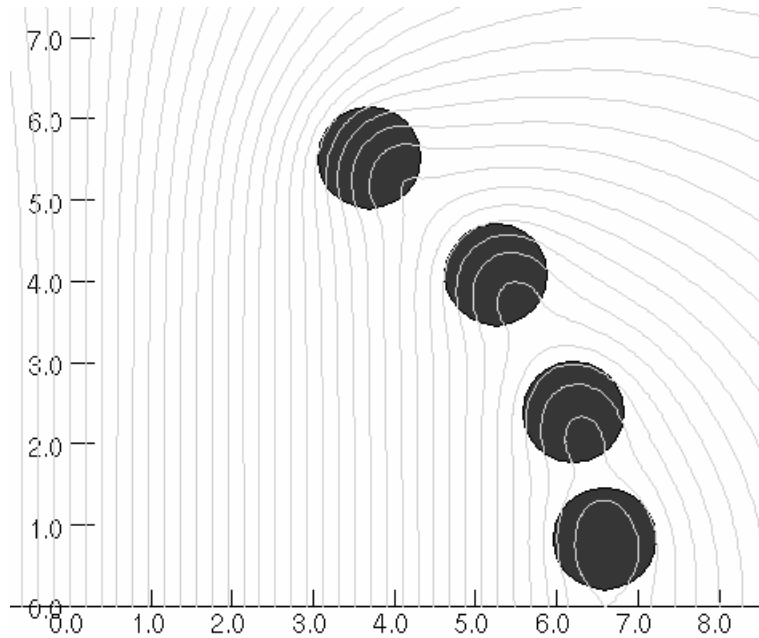
with ferrite



$$I_0 = 122.63 \text{ A}$$
$$L = 88.9 \text{ } \mu\text{H}$$

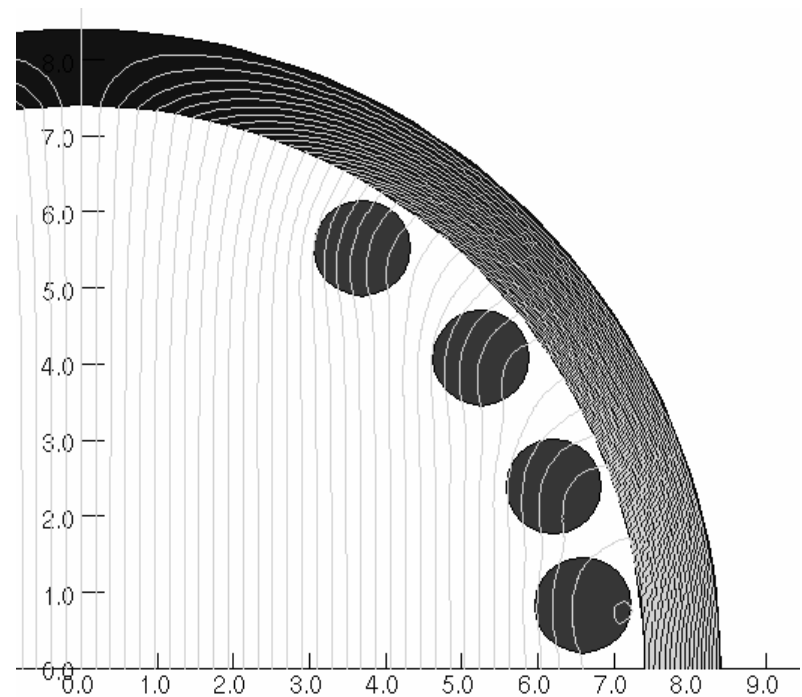
Cosine Theta Type – N=4 (x2)

Air-coil



$$I_0 = 264.7 \text{ A}$$
$$L = 32.2 \mu\text{H}$$

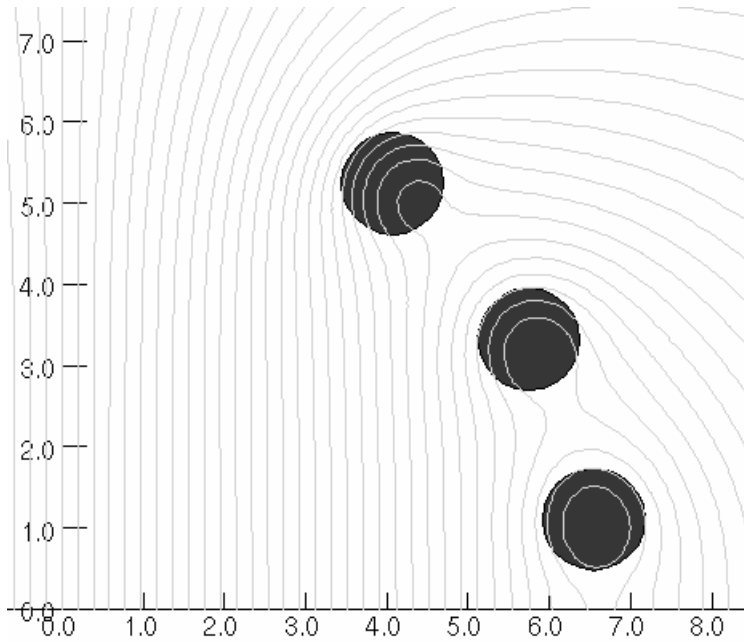
with ferrite



$$I_0 = 145.6 \text{ A}$$
$$L = 60.4 \mu\text{H}$$

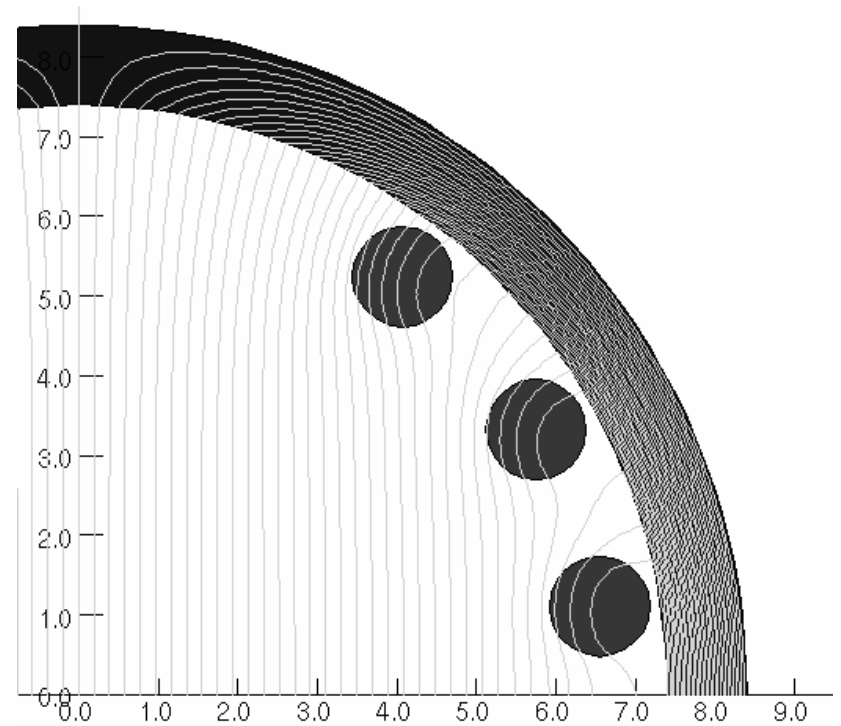
Cosine Theta Type – N=3 (x2)

Air-coil



$I_0 = 350.7 \text{ A}$
 $L = 18.8 \mu\text{H}$

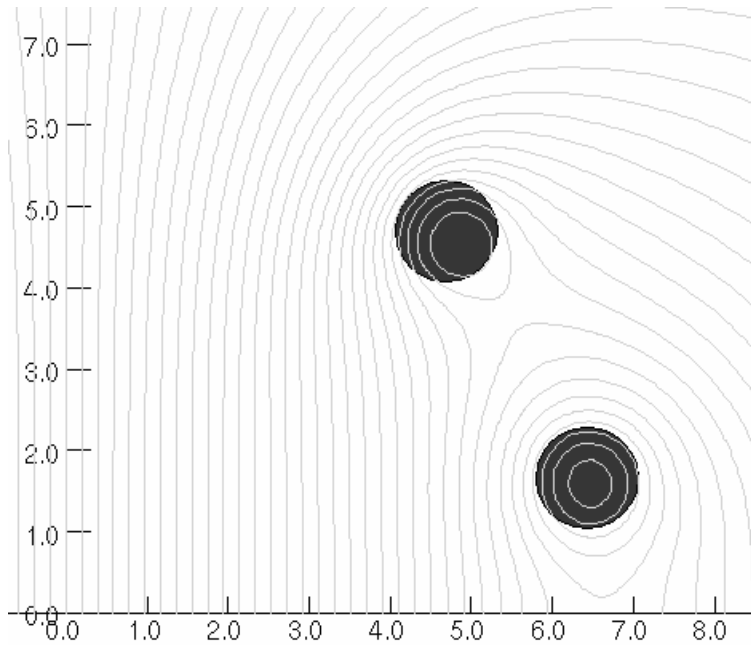
with ferrite



$I_0 = 192.9 \text{ A}$
 $L = 34.8 \mu\text{H}$

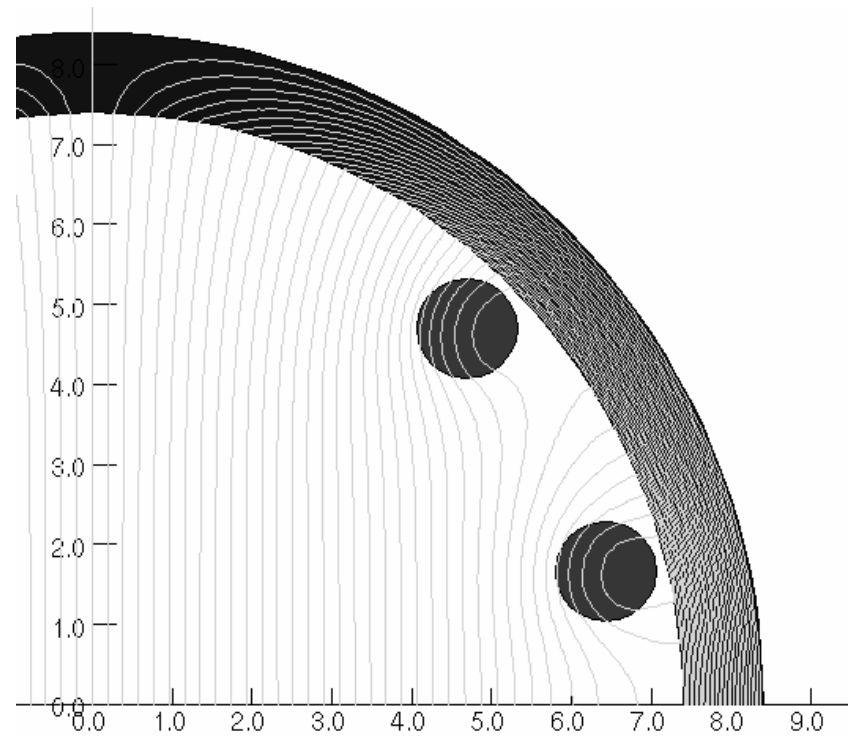
Cosine Theta Type – N=2 (x2)

Air-coil



$I_0 = 517.3 \text{ A}$
 $L = 9.2 \mu\text{H}$

with ferrite



$I_0 = 284.5 \text{ A}$
 $L = 16.7 \mu\text{H}$

Cosine Type Summary --

- (1) All the cases above (except cosine 7-turn one-layer) same conductors are used (as existing one: $d=0.5''$), tentatively
- (2) Ferrite shell reduces current by a factor of $\sim 0.52-0.55$; increases inductance by a factor of ~ 1.9 ; it gives slightly better field, and will make internal field stable in the tunnel
- (3) Comments ---
 - a. Less number of turns gives smaller inductance, but requires tight tolerance on conductor position random errors;
 - b. Real conductor (Litz wire) may contribute additional error due to the deformation of the strand/bundle;
 - c. Preference: with Ferrite shell (?).

(II) Window-frame Type –

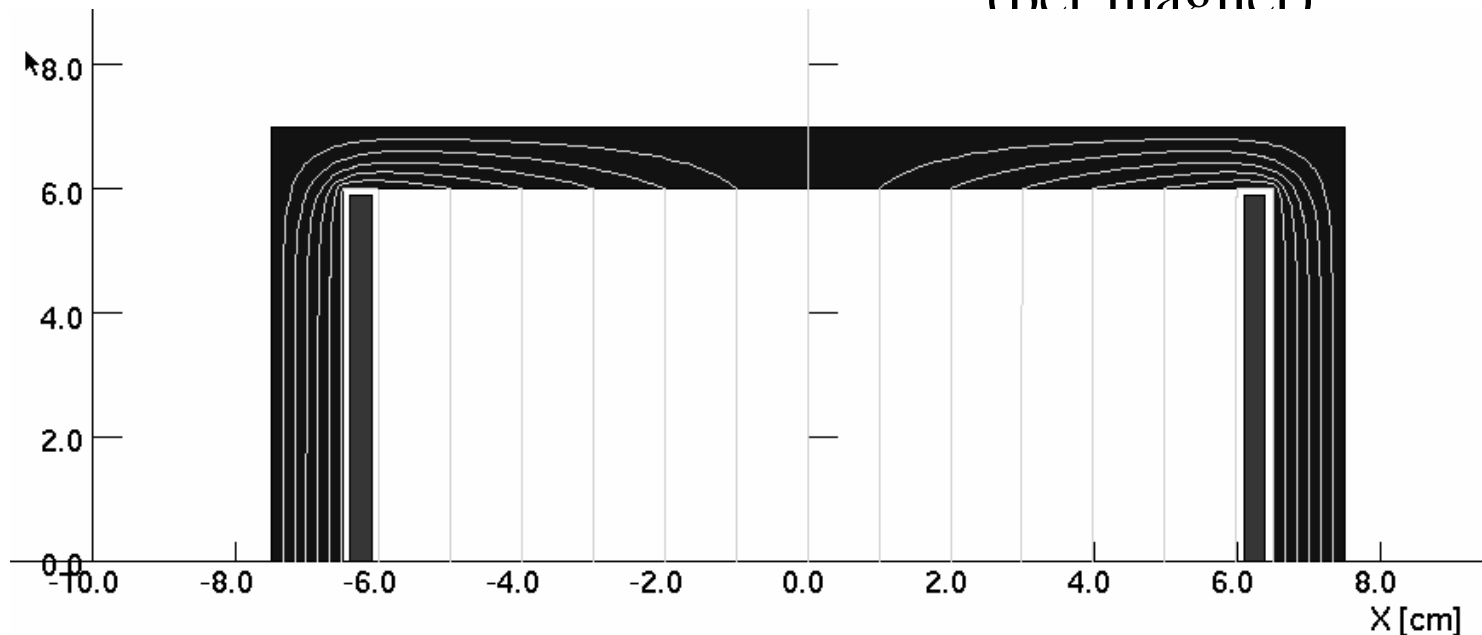
$$N=1 \text{ (x2)}$$

$$I_0 = 480 \text{ A}$$

$$L = 5.1 \text{ } \mu\text{H}$$

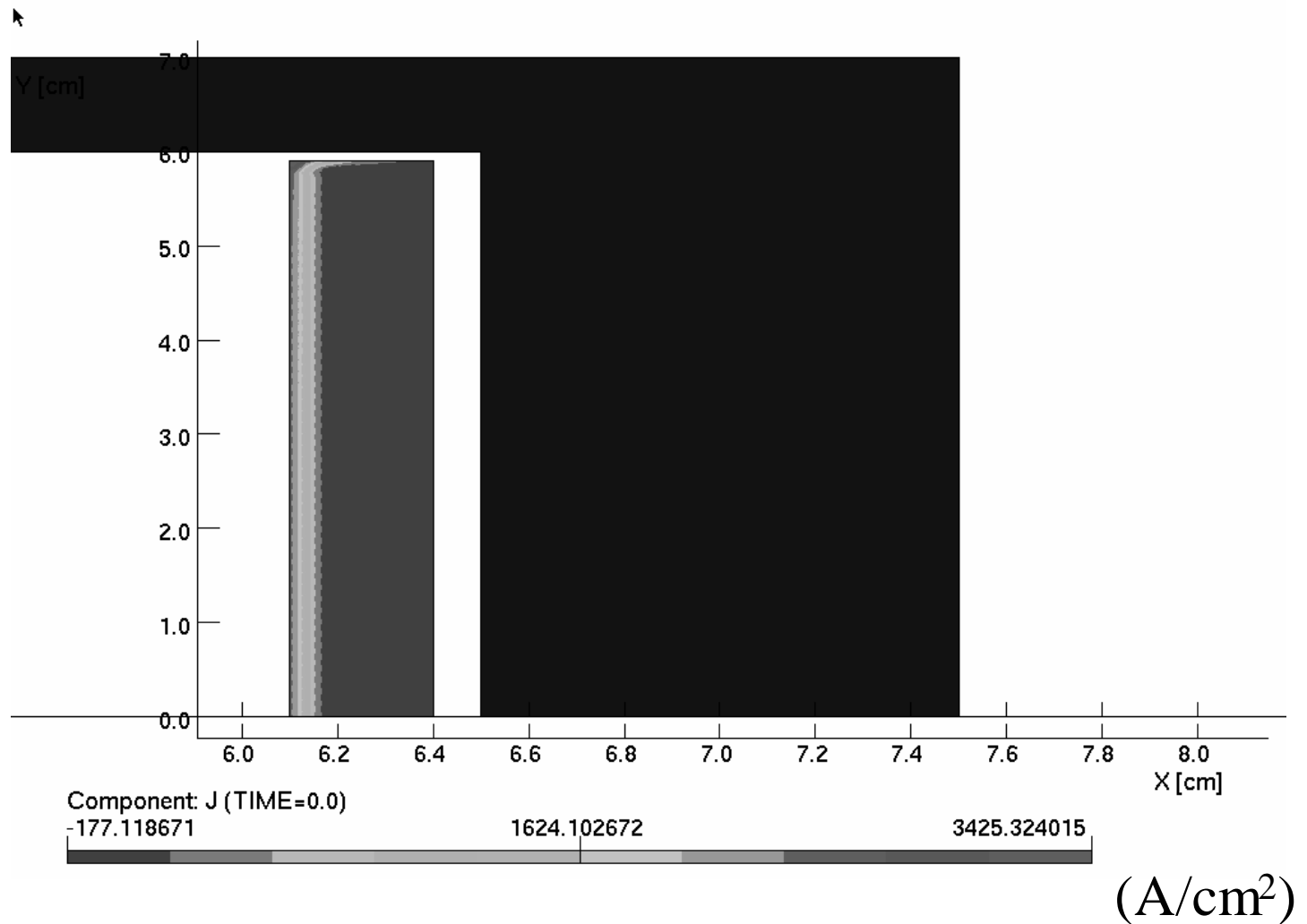
If use solid Cu stripes, loss in conductors: 400 W (39 kHz);
($P = ? J^2/s \text{ } ds$)

(near magnet)



Current density distribution in the Cu conductor ($f = 39 \text{ kHz}$)

$$I(t) = 480 * \cos(2\pi f t)$$



Window-frame Type Summary –

- (1) It gives good field control and small inductance;
- (2) The loss in the Cu conductor is an issue...